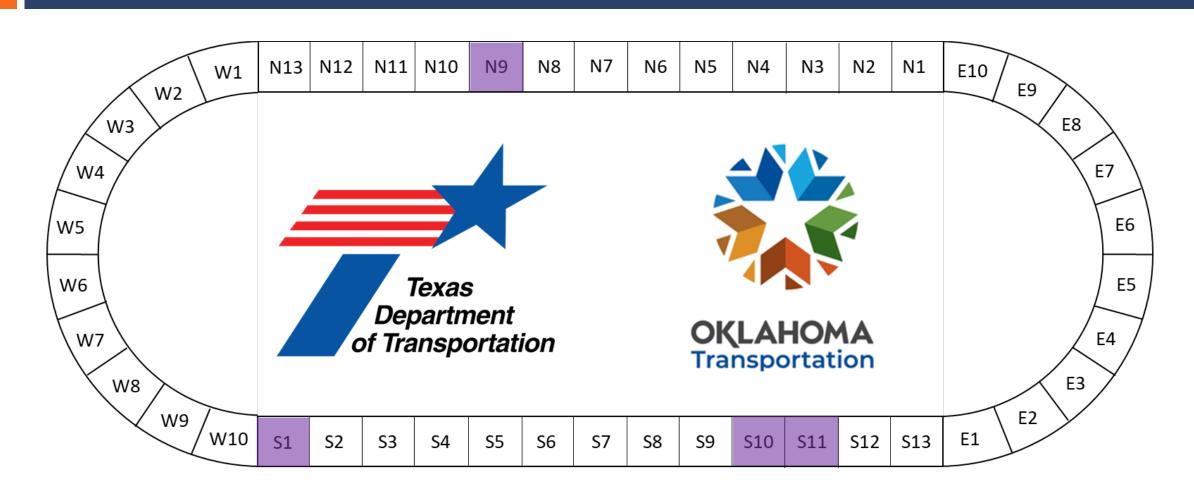


Balanced Mix Design (BMD) Experiments



Texas BMD Experiment



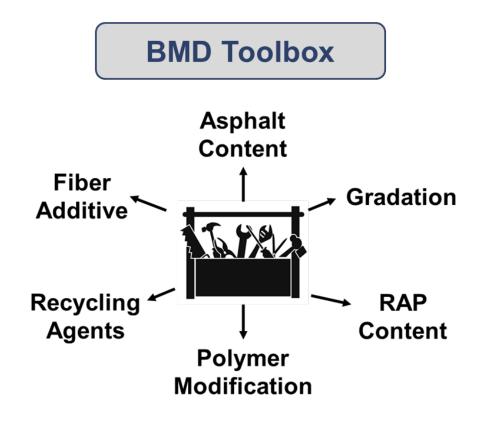
- Objective: performance comparison of asphalt mixes designed with a BMD approach versus the traditional volumetric approach
- □ 2.5-inch mill-and-inlays over existing pavements with 15 to 20% cracked lane area
- Mix designs
 - **■** 12.5 mm SP-C surface mix (50 gyrations)
 - **□** PG 70-22 SBS modified binder
 - **□** 20% RAP binder replacement ratio
 - **□** S11 volumetric mix
 - **□** S10 BMD mix (HWTT + OT)



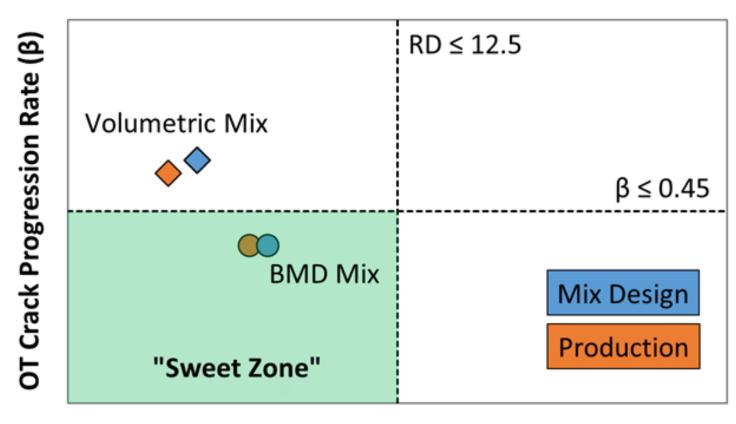
Mix Design Modifications for S10 BMD Mix

- Coarser gradation
- Higher VMA and V_{be}
- □ Improved cracking resistance
- Mix design volumetrics

Mix Property	S10 BMD	S11 Volumetric
Binder Content, %	5.5	4.7
Air Voids, %	4.0	4.0
VMA (G _{se}), %	16.6	15.0
V _{be} (G _{se}), %	12.6	11.0
VFA (G _{se}), %	76	73



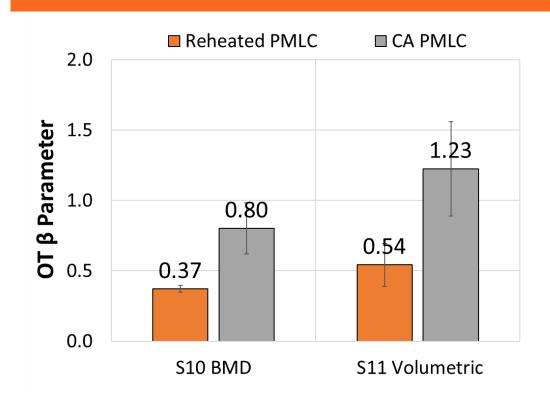
BMD Performance Testing



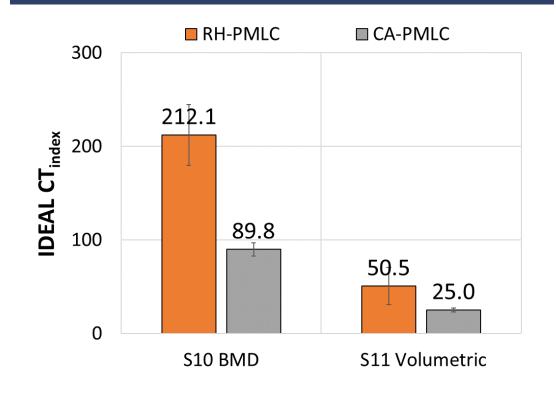
HWTT Rut Depth at 15k Passes (mm)

Impact of Mix Critical Aging (8 hours at 135°C)

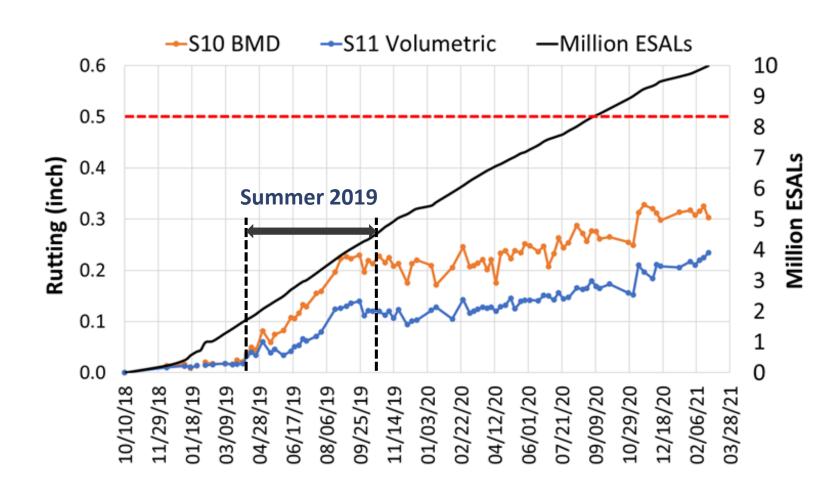




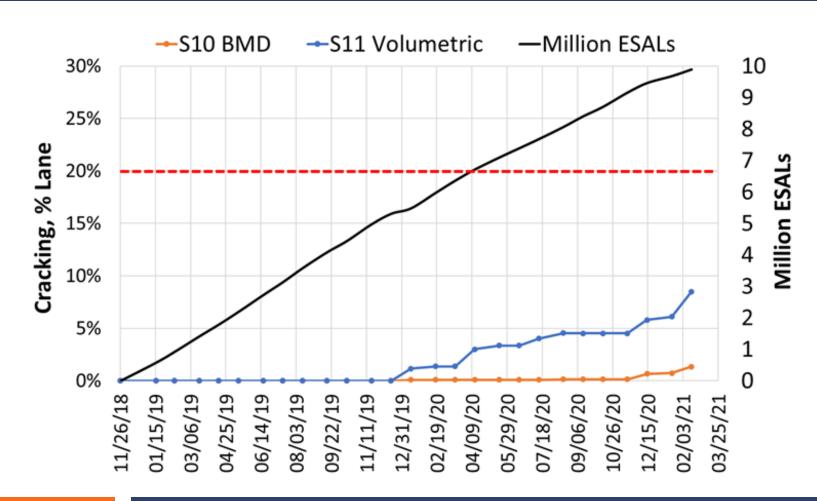
IDEAL Cracking Tolerance Index (CT_{Index})



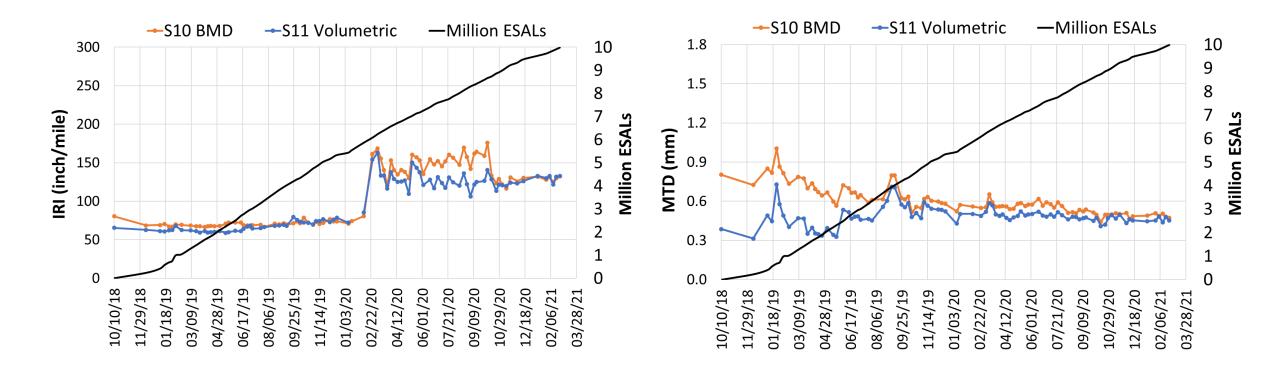
Rutting



Cracking



Smoothness and Texture



Conclusions and Recommendations

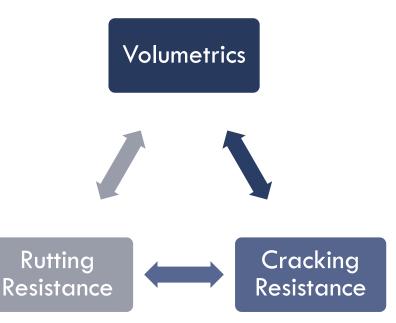
- Consistent performance test results from mix design and production testing
 - **□** S10 BMD: passed HWTT and OT
 - **□** S11 volumetric: passed HWTT, failed OT
- Significantly reduced cracking resistance after mix critical aging
 - □ S10 BMD > S11 volumetric
- □ Field performance after 10 million ESALs
 - **■** More rutting in S10 than S11
 - **■** More cracking & faster development rate in S11 than S10
 - **■** In agreement with BMD performance test results
 - **□** Similar smoothness, texture, and friction characteristics
- □ Traffic continuation to monitor longer-term performance



Oklahoma BMD Experiment



- Objective: implementation of mixture performance testing and criteria for BMD
- □ Section N9: 1.5-inch mill-and-inlay with a BMD mix
- Section S1: 5.0-inch mill-and-inlay with BMD surface and base mixes
- ODOT BMD approach
 - **□** Performance-Modified Volumetric Design
 - **□** HWTT for rutting evaluation
 - **□** I-FIT → IDEAL-CT for cracking evaluation
 - **□** Up to 15% RAP in surface mixes
 - 3 to 4% design air voids



Mix Designs

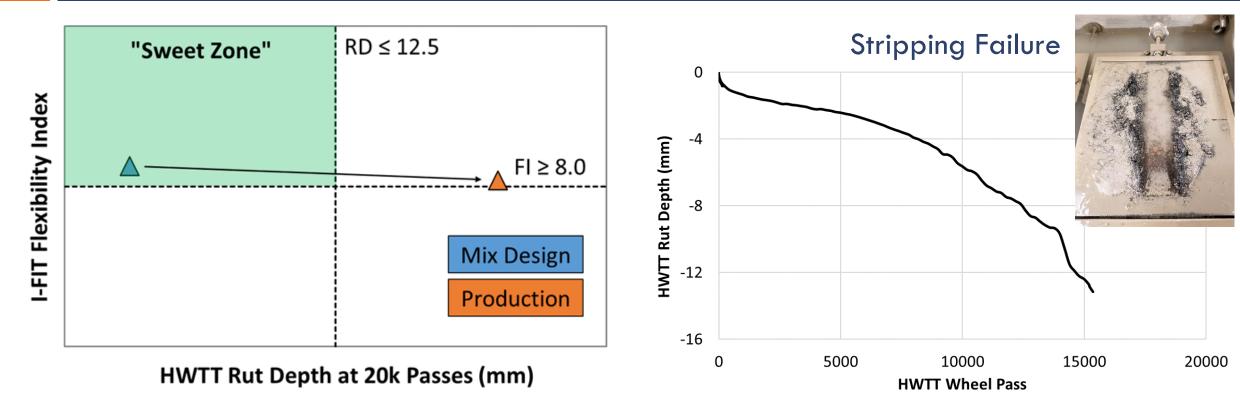
Section N9

- ODOT S5 mix (9.5 mm NMAS)
- □ PG 76-28 SBS modified binder
- □ 15% RAP
- □ 5.6% AC, 15.5% VMA at 80 gyrations

Section S1

- Surface
 - **D** ODOT S4 mix (12.5 mm NMAS)
 - □ PG 70-28 SBS modified binder
 - **□** 12% RAP
 - **□** 5.8% AC, 16.2% VMA at 65 gyrations
- □ Base
 - **D** ODOT S3 mix (19 mm NMAS)
 - **□** PG 64-28 SBS modified binder
 - 30% RAP + tall-oil based recycling agent
 - **■** 5.2% AC, 14.0% VMA at 65 gyrations

N9 BMD Performance Testing

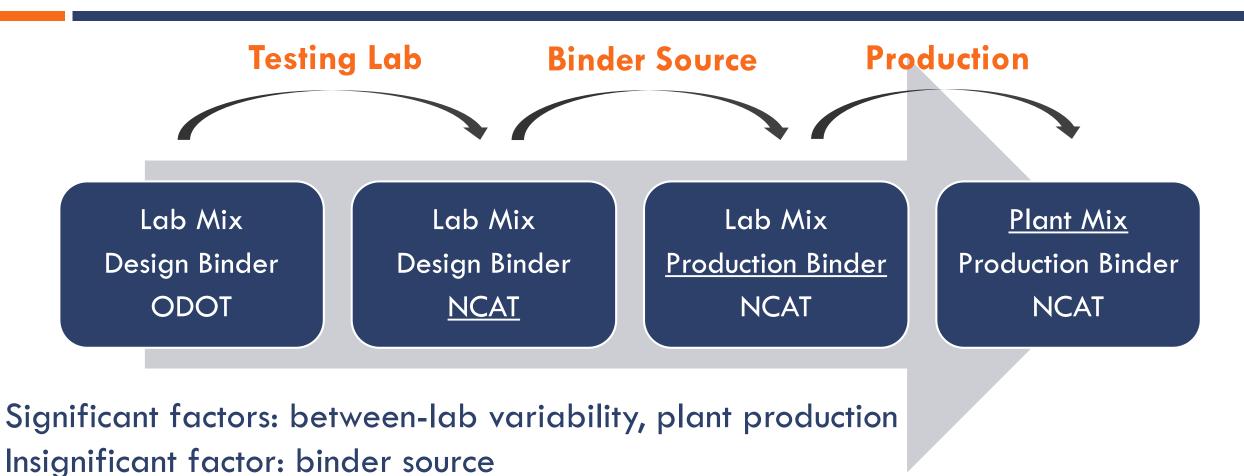


No concern for rutting failure based on HWTT Corrected Rut Depth (CRD) analysis, IDEAL-RT and HT-IDT testing

SEVENTH RESEARCH CYCLE

NCAT TEST TRACK CONFERENCE

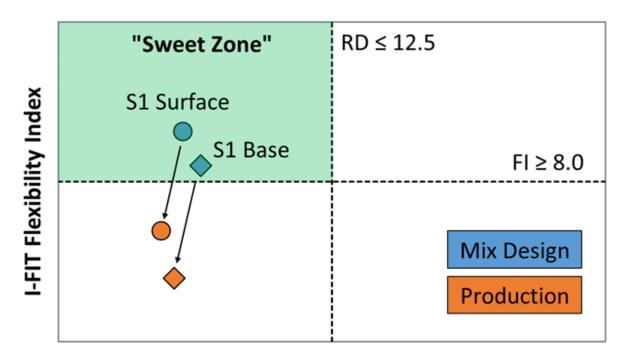
N9 Mix Design vs. Production Testing



SEVENTH RESEARCH CYCLE

NCAT TEST TRACK CONFERENCE

S1 BMD Performance Testing

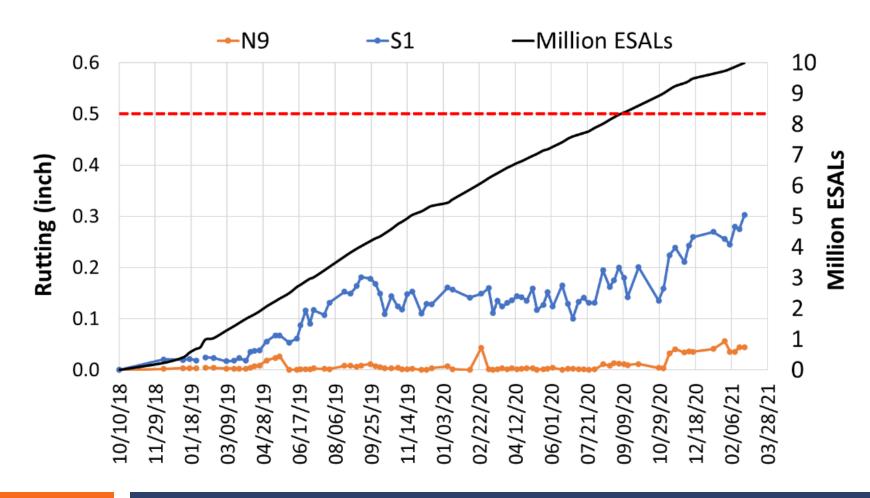


HWTT Rut Depth at 20k Passes (mm)

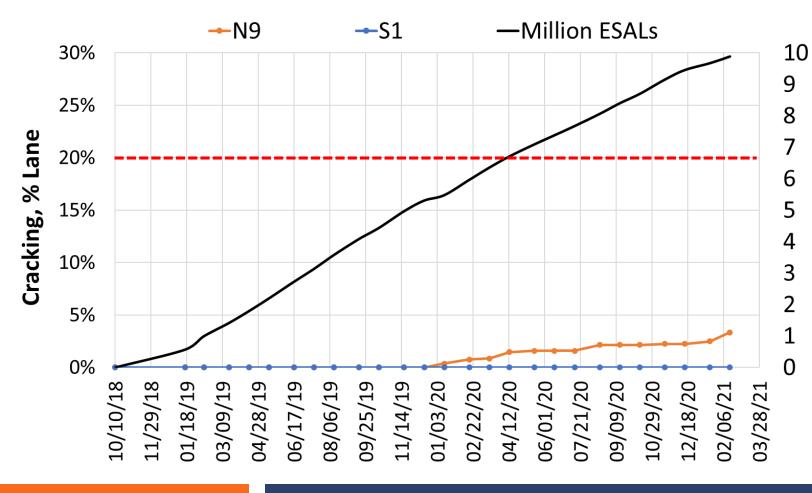
Additional I-FIT Testing

- Significant factor: plant production
- Insignificant factors: between-lab variability, binder source

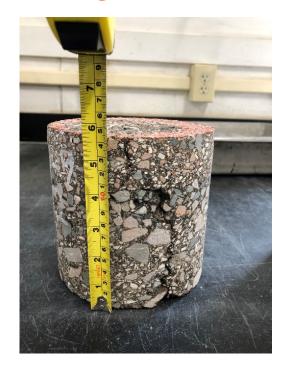
Rutting



Cracking



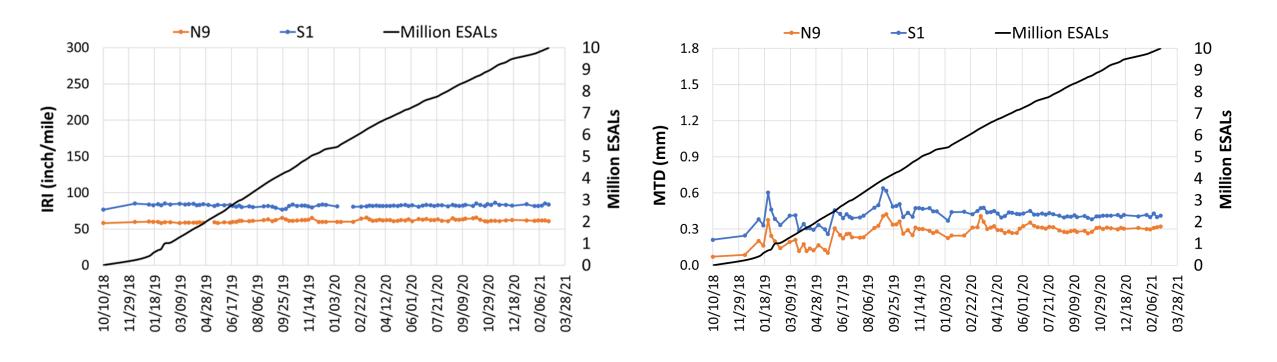
Cracking in Section N9



Million ESALs

SEVENTH RESEARCH CYCLE

Smoothness and Texture



Conclusions and Recommendations

- □ Production mixes failed mix design performance requirements
 - N9 failed HWTT due to stripping
 - **□** S1 failed I-FIT and IDEAL-CT
- Alternative HWTT analysis to discriminate rutting and striping failure
- □ Significant impacts of between-lab variably and plant production on mixture performance test results
 - Round robin and training on specimen fabrication and testing
 - **□** Performance testing during production
- □ Good field performance after 10 million ESALs
- □ Traffic continuation for S1 to monitor longer-term performance and verify IDEAL-CT criteria

Questions and Answers (f-yin@auburn.edu)

